



UNIVERSITÉ  
DE LORRAINE



POLYTECH<sup>®</sup>  
NANCY

*Data-driven model learning  
of dynamical systems*

-

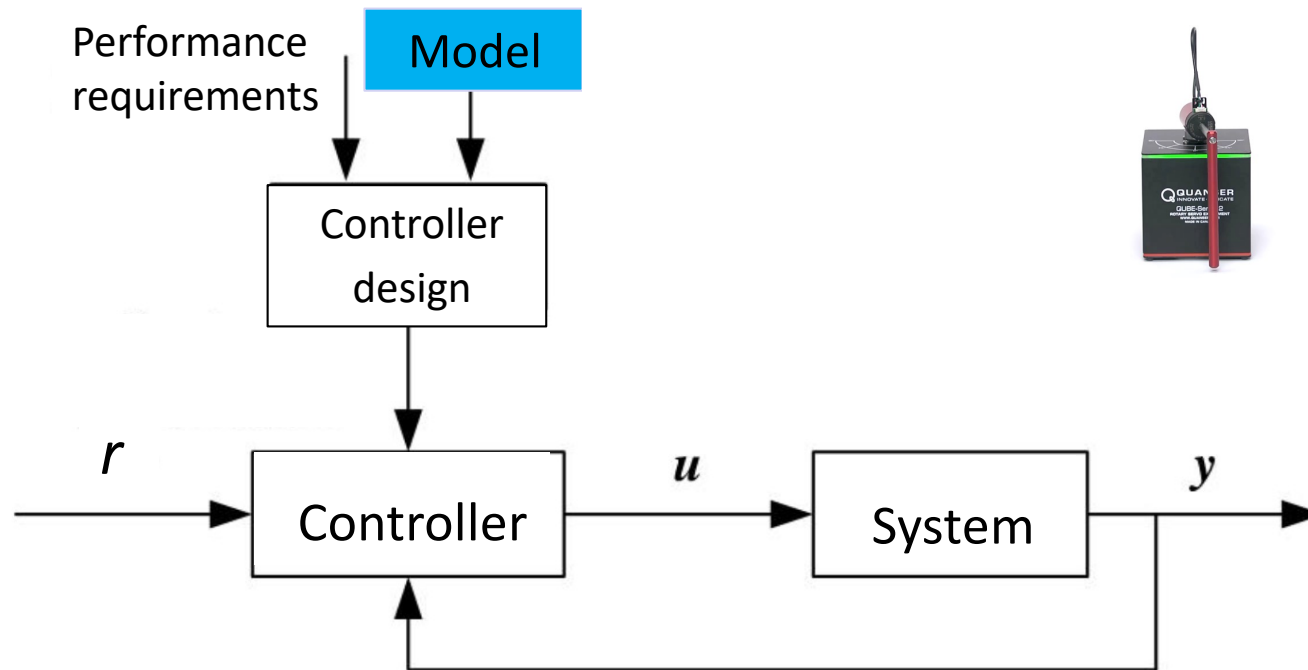
*A case study with the QUBE servo 2*

Hugues GARNIER

[hugues.garnier@univ-lorraine.fr](mailto:hugues.garnier@univ-lorraine.fr)

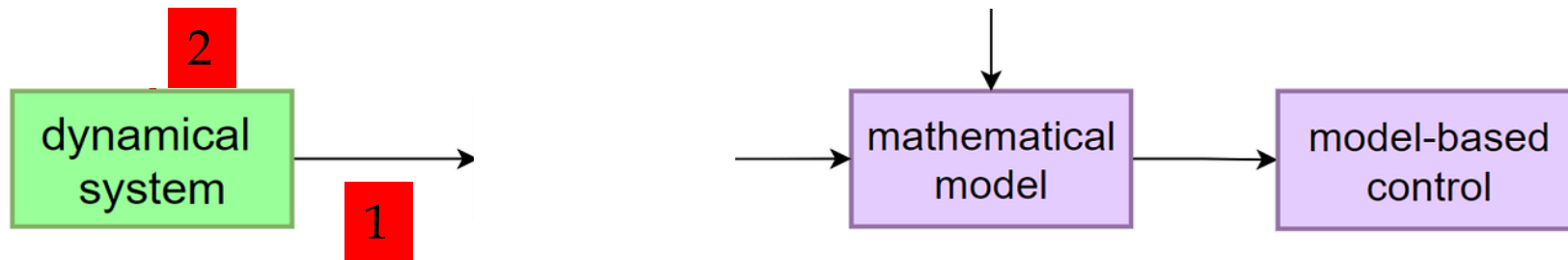
## Model identification for control What is it all about?

- Control is an interdisciplinary branch of engineering and mathematics that deals with dynamical systems with inputs, and how their behavior is modified by feedback



To do it in a **systematic way**, a *model-based approach for control design* has been developed

# The two main ways to determine a mathematical model for control design



# Model-based control design

## Case study: Rotary speed control of the QUBE servo 2



(a) QUBE-Servo 2 with Inertia Disc Module

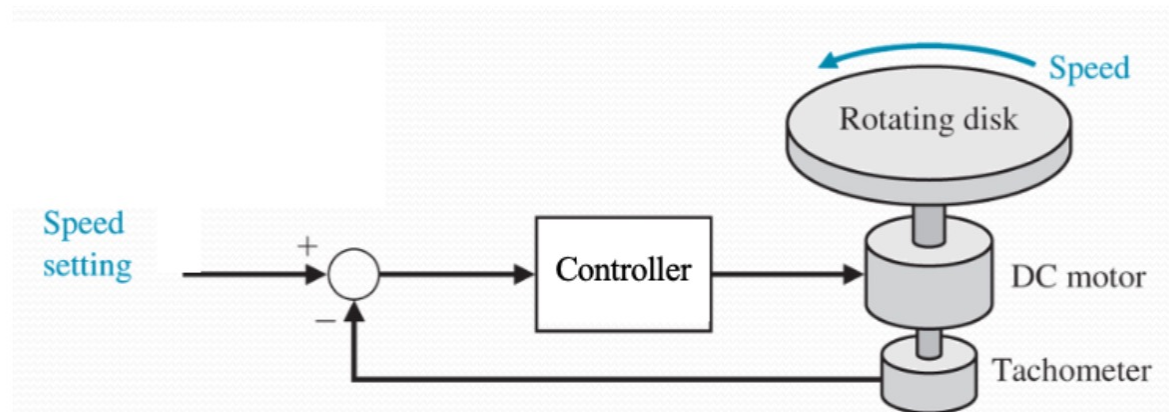
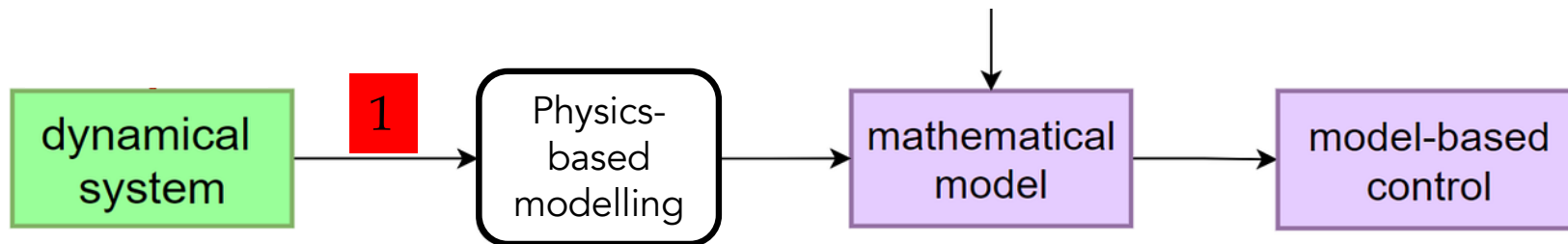
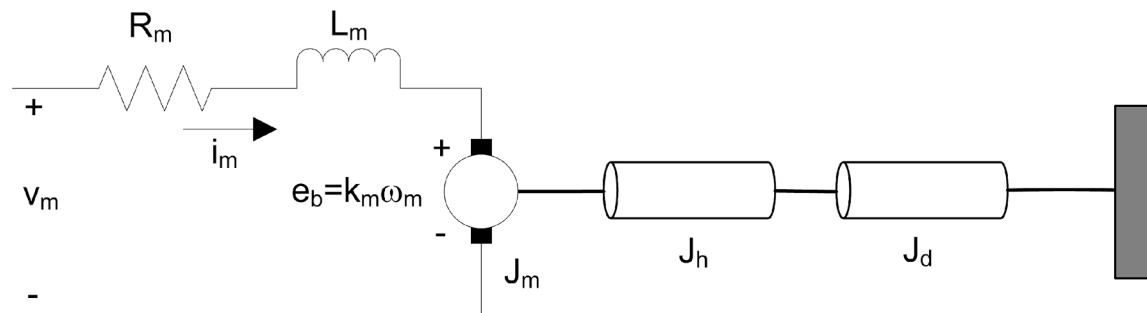


Figure 1.2: Schematic of the feedback speed control of the rotating disk

# First way to determine a mathematical model: Physics-based modelling



## Example: Physics-based modelling of the QUBE servo 2



(a) QUBE-Servo 2 with Inertia Disc Module

The equations of motion are:

$$R_m i_m(t) + L_m \frac{di_m(t)}{dt} = v_m(t) - k_m \dot{\theta}_m(t)$$

$$J_{eq} \ddot{\theta}_m(t) + b \dot{\theta}_m(t) = k_t i_m(t)$$

$$J_{eq} = J_m + J_h + J_d$$

$$= J_m + \frac{1}{2} m_h r_h^2 + \frac{1}{2} m_d r_d^2$$

Simplifying assumptions:

- Since the motor inductance  $L_m$  is much less than its resistance, it can be ignored
- The viscous coefficient  $b$  is assumed very small, it can be ignored
- Static friction effects neglected

## Input voltage-to angular velocity transfer function



$$\frac{\Omega_m(s)}{V_m(s)} = G(s) = \frac{k_t}{J_{eq}R_m s + k_t k_m}$$

$$G(s) = \frac{\frac{1}{k_m}}{1 + \frac{J_{eq}R_m}{k_t k_m} s}$$

$$G(s) = \frac{K}{Ts + 1}$$

$$K = \frac{1}{k_m}; \quad T = \frac{J_{eq}R_m}{k_t k_m}$$

## Example: Physical modelling of the QUBE servo 2

Physical parameters need to be determined from mechanical and electrical **datasheet** of the QUBE servo 2

Symbol	Description	Value
<b>DC Motor</b>		
$R_m$	Terminal resistance	8.4Ω
$k_t$	Torque constant	0.042 N.m/A
$k_m$	Motor back-emf constant	0.042 V/(rad/s)
$J_m$	Rotor inertia	4.0 × 10 <sup>-6</sup> kg.m <sup>2</sup>
$L_m$	Rotor inductance	1.16 mH
$m_h$	Load hub mass	0.0106 kg
$r_h$	Load hub mass	0.0111 m
$J_h$	Load hub inertia	0.6 × 10 <sup>-6</sup> kg.m <sup>2</sup>
<b>Load Disk</b>		
$m_d$	Mass of disk load	0.053 kg
$r_d$	Radius of disk load	0.0248 m



(a) QUBE-Servo 2 with Inertia Disc Module

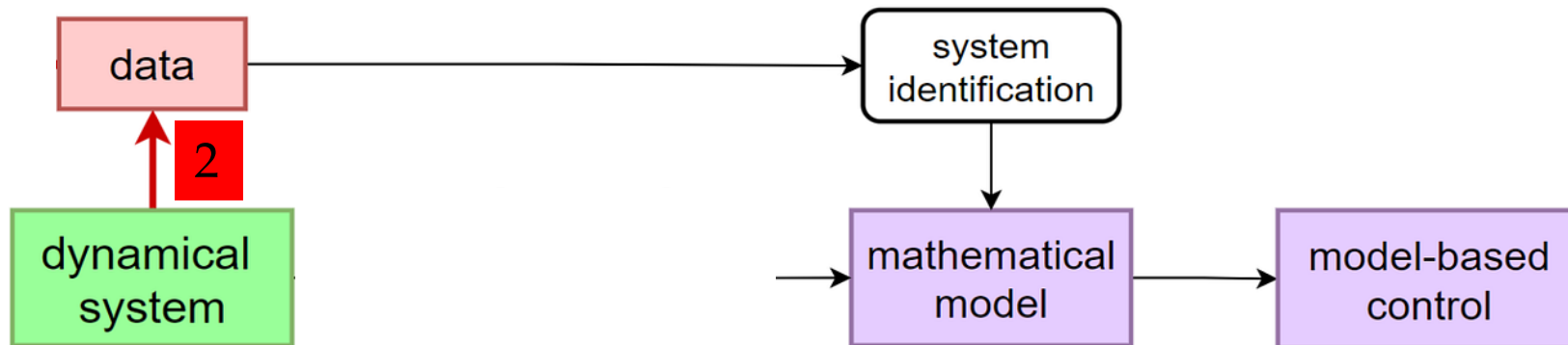
$$\begin{aligned}
 J_{eq} &= J_m + J_h + J_d \\
 &= J_m + \frac{1}{2} m_h r_h^2 + \frac{1}{2} m_d r_d^2
 \end{aligned}$$

Table 1.1: QUBE-Servo 2 system parameters

$$G(s) = \frac{\frac{1}{k_m}}{1 + \frac{J_{eq} R_m}{k_t k_m} s} = \frac{23.81}{1 + 0.0994s}$$

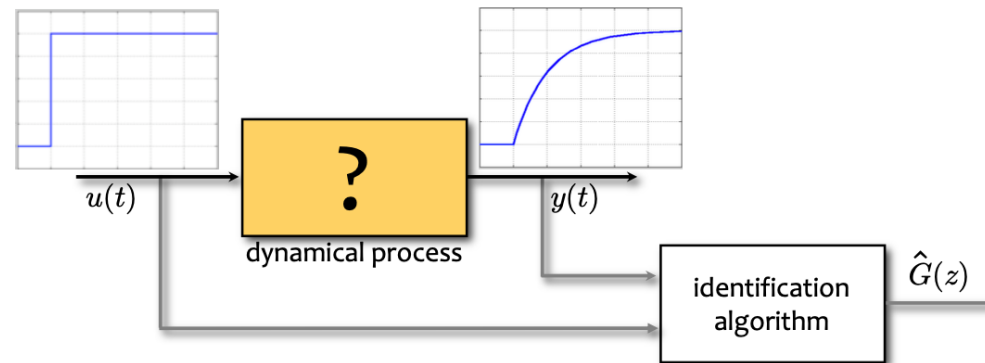


## Second way to determine a mathematical model: Data-driven system identification



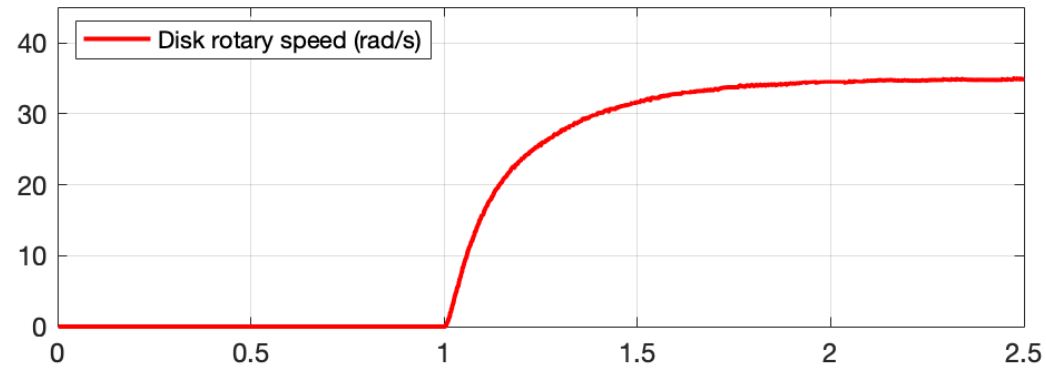
## Basic system identification method

### Step response-based model identification

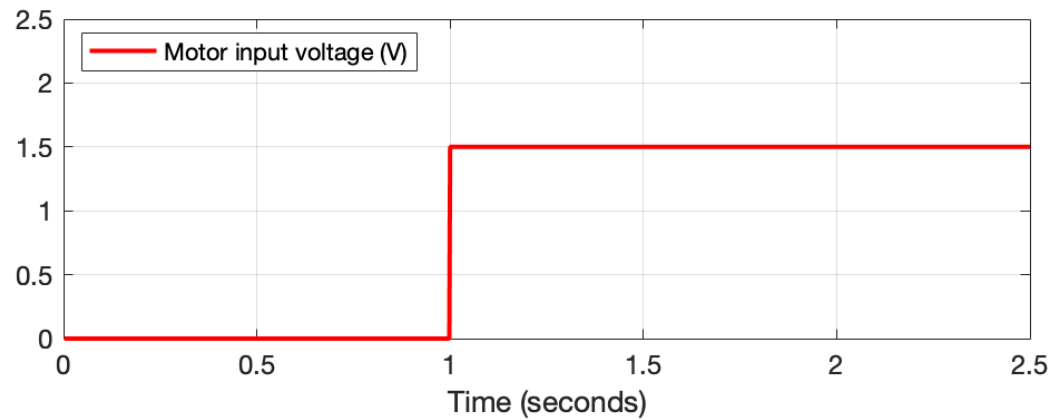


- Excite the process with a step  $u(t)$  , record output response  $y(t)$
- Observe the shape of  $y(t)$   
(1st-order response ? 2nd-order undamped response ? Any delay ? ...)

# Example: Step response identification of the QUBE servo 2



(a) QUBE-Servo 2 with Inertia Disc Module



## Example: Step response identification of the QUBE servo 2 by using the CONTSID toolbox

```
load data_step_Qube_speed
t=speed_data(1,:)'; % time-instants
y=speed_data(2,:)'; % rotary speed in rad/sec
u=speed_data(3,:)'; % motor input voltage in V
Ts=t(2)-t(1);      % Sampling period in sec

data=iddata(y,u,Ts);
idplot(data)

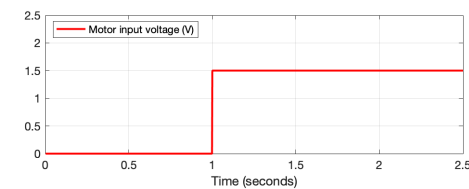
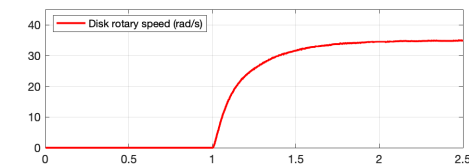
Model_type=idproc('P1'); % Simple first-order model
M=procsrivc(data,Model_type)
Process model with transfer function:

      Kp
G(s) = -----
      1+Tp1*s

      Kp = 22.98
      Tp1 = 0.18072
```

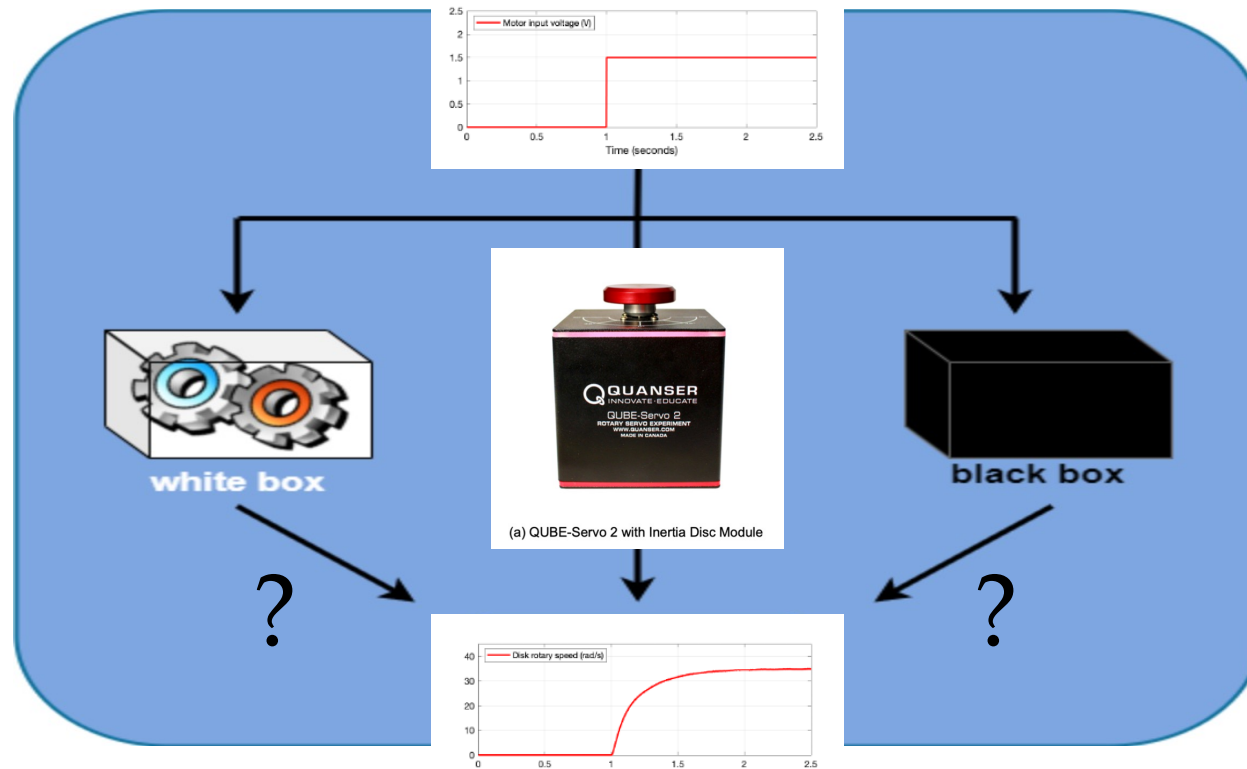


(a) QUBE-Servo 2 with Inertia Disc Module

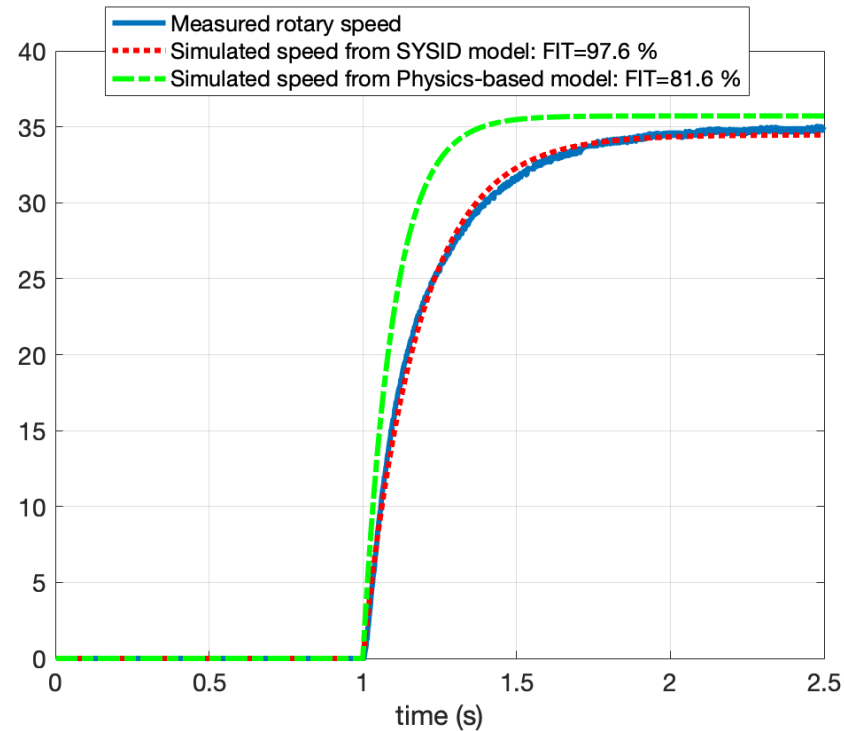


# Model quality assessment

Let us compare the measured and model outputs for the step input



## Comparison of the physics-based and identified models



(a) QUBE-Servo 2 with Inertia Disc Module

The fit is better for the System identification (SYSID) black-box model

Why is there a discrepancy for the Physics-based white-box model? Possible reasons:

- Physical parameters have tolerances and may be slightly off
- Un-modeled effects such as motor inductance,...

The two models capture quite well the main dynamic of the QUBE servo 2 system

*Any of the two models could be used to design a PI control with good performance*