Adaptive observer for fault estimation in nonlinear systems described by a Takagi-Sugeno model

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18th Mediterrranean Conference on Control and Automation.

Marrakech, Morocco, 23-25th, 2010







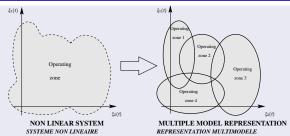


Outline

- Multiple model structures
- Pault estimation
- 3 Example
- Conclusion and future works

Multiple model structures

Principle of the multiple models



- Operating range decomposition into a finite number of operating zones
- Each operating zone is modelled using a simple linear submodel
- The relative contribution of each submodel is quantified by a weighting function
- The global nonlinear model is the sum of the submodels weighted by these functions

Advantages of multiple models

- Well approximate the behaviour of the complex nonlinear systems
- Several results for linear systems can be extended to nonlinear systems through this kind of models

Takagi-Sugeno model

Structure of the model

Multiple model with a unique state

$$\begin{cases} \dot{x}(t) = \sum_{i=1}^{M} \mu_i(\xi(t))(A_ix(t) + B_iu(t)) \\ y(t) = \sum_{i=1}^{M} \mu_i(\xi(t))C_ix(t) = Cx(t) \end{cases}$$

$$\mu_{i}(\xi(t)) \begin{cases} \sum_{i=1}^{M} \mu_{i}(\xi(t)) = 1, & \forall t & \xi(t) : decision \ variable \\ 0 \leq \mu_{i}(\xi(t)) \leq 1, & \forall t, \ \forall i \in \{1, ..., M\} \end{cases}$$

- The local models share the same state vector
- The output equation is frequently assumed linear (all the matrices C_i are equal)

Problem formulation

System affected by actuator and sensor faults + output noise

$$\begin{cases} \dot{x}(t) = \sum_{i=1}^{M} \mu_i(\xi(t))(A_ix(t) + B_iu(t) + \frac{E_if_a(t)}{E_if_a(t)}) \\ y(t) = Cx(t) + \frac{F_if_a(t)}{E_if_a(t)} \end{cases}$$

Objective: transform the original sensor faults into actuator faults

z(t): filtered version of the output y(t)

$$\dot{z}(t) = \sum_{i=1}^{M} \mu_i(\xi(t))(-\overline{A}_i z(t) + \overline{A}_i(Cx(t) + Ff_s(t) + Dw(t)))$$

 $-\bar{A}_i$: stable matrices

Problem formulation

Augmented state and fault vector

$$X = \begin{bmatrix} x \\ z \end{bmatrix}, \quad f = \begin{bmatrix} f_a \\ f_s \end{bmatrix}$$

Augmented system

$$\begin{cases} \dot{X}(t) = \sum_{i=1}^{M} \mu_{i}(\xi(t))(A_{ai}X(t) + B_{ai}u(t) + E_{ai}f(t)) + F_{ai}w(t)) \\ Y(t) = C_{a}X(t) \end{cases}$$

$$A_{ai} = \begin{bmatrix} A_{i} & 0 \\ \bar{A}_{i}C & -\bar{A}_{i} \end{bmatrix}, B_{ai} = \begin{bmatrix} B_{i} \\ 0 \end{bmatrix}, E_{ai} = \begin{bmatrix} E_{i} & 0 \\ 0 & \bar{A}_{i}F \end{bmatrix}, F_{ai} = \begin{bmatrix} 0 \\ \bar{A}_{i}D \end{bmatrix}$$

$$C_{a} = \begin{bmatrix} 0 & I \end{bmatrix}$$

Re-written system in an augmented form

$$\begin{cases} \dot{X}(t) = \sum_{i=1}^{M} \mu_{i}(\xi(t))(A_{ai}X(t) + B_{ai}u(t) + E_{ai}f(t) + F_{ai}w(t)) \\ Y(t) = C_{a}X(t) \end{cases}$$

Proportional integral observer

$$\begin{cases} \dot{\hat{X}}(t) = \sum_{i=1}^{M} \mu_{i}(\xi(t))(A_{ai}\hat{X}(t) + B_{ai}u(t) + E_{ai}\hat{f}(t) + K_{i}(Y(t) - \hat{Y}(t))) \\ \dot{\hat{f}}(t) = \sum_{i=1}^{M} \mu_{i}(\xi(t))(L_{i}(Y(t) - \hat{Y}(t))) \\ \hat{Y}(t) = C_{a}\hat{X}(t) \end{cases}$$

Estimation errors

$$\tilde{x}(t) = X(t) - \hat{X}(t)$$
 and $\tilde{f}(t) = f(t) - \hat{f}(t)$

Dynamics of the errors

$$\dot{\tilde{x}}(t) = \sum_{i=1}^{M} \mu_i(\xi(t))((A_{ai} - K_iC_a)\tilde{x}(t) + E_{ai}\tilde{f}(t) + F_{ai}w(t))$$

$$\dot{\tilde{f}}(t) = \dot{f}(t) - \sum_{i=1}^{M} \mu_i(\xi(t)) L_i C_a \tilde{x}(t)$$

Augmented system of estimation errors

The following vectors are introduced:

$$arphi(t) = \left[egin{array}{c} ilde{x}(t) \ ilde{f}(t) \end{array}
ight] ext{ and } arepsilon(t) = \left[egin{array}{c} w(t) \ ilde{f}(t) \end{array}
ight]$$

Augmented system of estimation errors

$$\dot{\varphi}(t) = A_m \varphi(t) + B_m \varepsilon(t)$$

with:
$$A_m = \sum_{i=1}^M \mu_i(\xi(t)) \tilde{A}_{0i}$$
 and $B_m = \sum_{i=1}^M \mu_i(\xi(t)) \tilde{B}_{0i}$,

$$\tilde{A}_{0i} = \left[egin{array}{cc} A_{ai} - K_i C_a & E_{ai} \\ -L_i C_a & 0 \end{array}
ight], \ \tilde{B}_{0i} = \left[egin{array}{cc} F_{ai} & 0 \\ 0 & I \end{array}
ight]$$

Convergence of the generalized estimation error

Let us consider the following quadratic Lyapunov candidate function:

$$V(t) = \varphi^T(t)P\varphi(t)$$

Robust state and fault estimation

Convergence conditions

The problem of robust state and fault estimation is reduced to find the gains K_i and L_i of the observer to ensure an asymptotic convergence of $\varphi(t)$ towards zero if $\varepsilon(t)=0$ and to ensure a bounded error in the case where $\varepsilon(t)\neq 0$, i.e. :

$$\lim_{t \to \infty} \varphi(t) = 0$$
 for $\varepsilon(t) = 0$ $\|\varphi(t)\|_{Q_{\varphi}} \le \lambda \|\varepsilon(t)\|_{Q_{\varepsilon}}$ for $\varepsilon(t) \ne 0$

where $\lambda > 0$ is the attenuation level.

To satisfy these constraints, it is sufficient to find a Lyapunov function V(t) such that

$$\dot{V}(t) + \varphi^{T}(t)Q_{\varphi}\varphi(t) - \lambda^{2}\varepsilon^{T}(t)Q_{\varepsilon}\varepsilon(t) < 0$$

Robust state and fault estimation

Augmented system

$$\dot{\varphi}(t) = A_m \varphi(t) + B_m \varepsilon(t)$$

$$\dot{V}(t) + \varphi^{T}(t)Q_{\varphi}\varphi(t) - \lambda^{2}\varepsilon^{T}(t)Q_{\varepsilon}\varepsilon(t) < 0$$

Omitting to denote t, the last inequality can also be written as:

$$\psi^T \Omega_m \psi < 0$$

with:

$$\psi = \left[egin{array}{c} \varphi \ arepsilon \end{array}
ight] \ \ ext{and} \ \ \Omega_m = \left[egin{array}{c} A_m^T P + P A_m + Q_{\phi} & P B_m \ B_m^T P & -\lambda^2 Q_{arepsilon} \end{array}
ight]$$

This inequality holds if $\Omega_m < 0$.

Robust state and fault estimation

LMI formulation

$$A_m = \sum_{i=1}^M \mu_i(\xi(t))\tilde{A}_{0i}, \qquad \tilde{A}_{0i} = \tilde{A}_i - \tilde{K}_i\tilde{C}$$

where:

$$\tilde{A}_{i} = \begin{bmatrix} A_{ai} & E_{ai} \\ 0 & 0 \end{bmatrix}, \quad \tilde{K}_{i} = \begin{bmatrix} K_{i} \\ L_{i} \end{bmatrix}, \quad \tilde{C} = \begin{bmatrix} C_{a} & 0 \end{bmatrix}$$

With the changes of variables $G_i = P\tilde{K}_i$ and $m = \lambda^2$, the matrix Ω_m can be written as :

$$\Omega_m = \sum_{i=1}^M \mu_i(\xi(t))\Omega_i$$

$$\Omega_{i} = \left[\begin{array}{cc} P\tilde{A}_{i} + \tilde{A}_{i}^{T}P - G_{i}\tilde{C} - \tilde{C}^{T}G_{i}^{T} + Q_{\phi} & P\tilde{B}_{0i} \\ \tilde{B}_{0i}^{T}P & -mQ_{\varepsilon} \end{array} \right]$$

Main result

Theorem

The system : $\dot{\varphi} = A_m \varphi + B_m \varepsilon$ describing the time evolution of the state estimation error \tilde{x} and the fault estimation error \tilde{f} is stable and the \mathscr{L}_2 -gain of the transfer from $\varepsilon(t)$ to $\varphi(t)$ is bounded, if there exists a symmetric, positive definite matrix P, gain matrices G_i , $i \in \{1...M\}$ and a positive scalar m such that the following LMI are verified :

$$\left[\begin{array}{cc} P\tilde{A}_i + \tilde{A}_i^T P - G_i \tilde{C} - \tilde{C}^T G_i^T + Q_{\phi} & P\tilde{B}_{0i} \\ \tilde{B}_{0i}^T P & -mQ_{\epsilon} \end{array}\right] < 0$$

The proportional and integral gains of the observer are computed using $\tilde{K}_{mi} = P^{-1}G_i$ and the attenuation level is given by $\lambda = \sqrt{m}$.

System matrices

$$A_{1} = \begin{bmatrix} -0.3 & -3 & -0.5 & 0.1 \\ -0.7 & -5 & 2 & 4 \\ 2 & -0.5 & -5 & -0.9 \\ -0.7 & -2 & 1 & -0.9 \end{bmatrix}, A_{2} = \begin{bmatrix} -0.7 & -7 & -1.5 & -7 \\ -0.2 & -2 & 0.6 & 1.3 \\ 5 & -1.5 & -9 & -3.9 \\ -0.4 & -1 & -0.3 & -1 \end{bmatrix}$$

$$B_{1} = \begin{bmatrix} 1 & 2 \\ 5 & 1 \\ 4 & -3 \\ 1 & 0 \end{bmatrix}, B_{2} = \begin{bmatrix} 1 & 1 \\ 2 & 1 \\ 0 & 2 \\ -1 & -2 \end{bmatrix}, D = \begin{bmatrix} 0.5 & 0.5 \\ 0.2 & 0.2 \\ 0.1 & 0.1 \\ 0 & 0.1 \end{bmatrix}, F = \begin{bmatrix} 3.25 & 5 \\ 0 & 0.5 \\ -3.25 & 1.75 \\ 5.75 & 5 \end{bmatrix}$$

$$E_{1} = B_{1}, E_{2} = B_{2}, C = I, \xi(t) = u(t)$$

$$Q_{\varphi} = Q_{\varepsilon} = I, \quad \bar{A}_1 = 5 \times I, \quad \bar{A}_2 = 10 \times I$$

Input signals

$$u(t) = \left[\begin{array}{c} u_1(t) \\ u_2(t) \end{array} \right] \left\{ \begin{array}{c} u_1(t) : \text{telegraph type signal whose amplitude belongs to } [0,0.5] \\ u_2(t) : 0.4 + 0.25 \sin(\pi t) \end{array} \right.$$

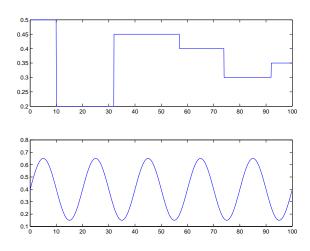


FIGURE: System inputs u(t)

Actuator and sensor faults

Actuator fault is defined as follows:

$$f_{a}(t) = \left[\begin{array}{c} f_{a1}(t) \\ f_{a2}(t) \end{array} \right]$$

with:

$$f_{a1}(t) = \begin{cases} 0.4\sin(\pi t), & 15 \text{ s} < t < 75 \text{ s} \\ 0, & \text{otherwise} \end{cases}, f_{a2}(t) = \begin{cases} 0, & t < 20 \text{ s} \\ 0.3, & 20 \text{ s} < t < 80 \text{ s} \\ 0.5, & t > 80 \text{ s} \end{cases}$$

and the sensor fault $f_s(t)$ is defined as follows:

$$f_{S}(t) = \left[\begin{array}{c} f_{S1}(t) \\ f_{S2}(t) \end{array} \right]$$

with:

$$f_{\rm S1}(t) = \left\{ \begin{array}{ll} 0, & t \leq 35 \ {\rm s} \\ 0.6, & t > 35 \ {\rm s} \end{array} \right., \ f_{\rm S2}(t) = \left\{ \begin{array}{ll} 0, & t \leq 25 \ {\rm s} \\ \sin(0.6\pi t), & t > 25 \ {\rm s} \end{array} \right.$$

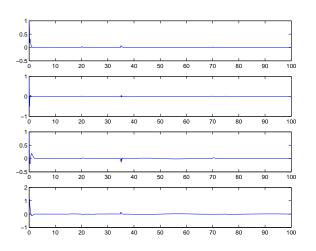


FIGURE: State estimation errors

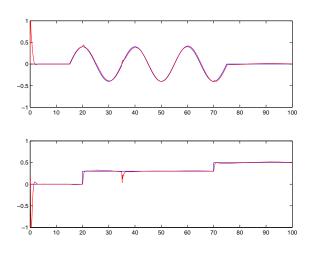


FIGURE: Actuator faults and their estimation

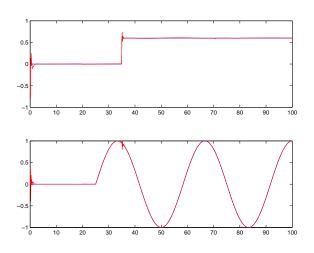


FIGURE: Sensor faults and their estimation

Conclusion and future works

Conclusion and future works

Conclusion

- Original method for state and fault estimation for systems described by nonlinear Takagi-Sugeno models using a proportional integral observer
- Using an adequate rewritting of the system equations, the sensor fault affecting the initial system is transformed into an actuator fault (i.e. into an unknown input); this transformation eases the simultaneous sensor and actuator fault estimation.

Future works

- Fault estimates can be used to conceive a fault tolerant control strategy able to cancel the fault effects on the system performances and behavior
- The proposed method should be extended to TS models with unmeasurable decision variables

Get in touch



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